



This example is designed to compare engineers' assumptions about water pressures acting on the face of a basement wall. The wall will NOT be provided with a drainage system. Ground surface behind the wall is horizontal will be paved in the long term.

The natural water level has been measured in local standpipes as follows:

Standpipe 1, distance x = 10m behind the wall, depth to water  $d_w = 2.2 m$ Standpipe 2, distance x = 25m behind the wall, depth to water  $d_w = 1.5 m$ Standpipe 3, distance x = 50m behind the wall, depth to water  $d_w = 3.1 m$ 

Three situations are envisaged (with different materials involved):

Situation A: natural ground = clay, fill = clay fill (from excavated natural ground) Natural clay:  $\gamma_k = 22 \text{ kN/m}^3$ ,  $c_{u,k} = 35 \text{ kPa}$ ,  $\phi'_k = 25^\circ$ ,  $c'_k = 0 \text{ kPa}$ 

- Situation B: natural ground = clay, fill = imported granular fill Natural clay: as above Imported granular fill:  $\gamma_k = 18 \text{ kN/m}^3$ ,  $\phi'_k = 35^\circ$ ,  $c'_k = 0 \text{ kPa}$
- Situation C: natural ground = gravel, fill = imported granular fill Natural gravel:  $\gamma_k = 19 \text{ kN/m}^3$ ,  $\phi'_k = 40^\circ$ ,  $c'_k = 0 \text{ kPa}$ Imported granular fill: as above

For each situation A-C above, please determine:

1) The characteristic depth of the water table  $d_{w,k}$ 

2) The characteristic thrust on the wall (over height H) owing to water pressures alone3) The characteristic thrust on the wall (over height H) owing to effective earth pressures alone

Repeat 1-3 above using design values for the serviceability limit state (SLS) Finally, repeat 1-3 above using design values for the ultimate limit state (ULS)